

Best of luck for your exam!  
Lm Hanye.

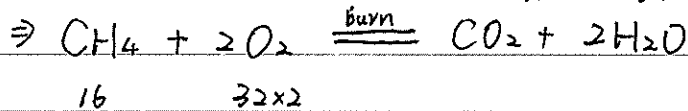
- Q.1. (a) Slow speed engine is the type of engine has these advantages:
- Rotation speed 80-330 rpm, no reduction gearbox is required
  - Direct drive to FPP
  - High output power capacity up to 80 MW.
  - Reversible
  - Best thermal efficiency (47% - 55%) and SFC = 170 kg only.
  - Can burn low quality fuel with good part load efficiency
  - Reliable (low technology requirement means lower wear & tear and maintenance requirement, hence, costs).

It used in large vessel such as dry bulk and container vessel although it still have disadvantages of longer starting and stop time and big cylinder cycle needed.

(b)  $\text{CH}_4$ : 16 kg/kmol

$\text{O}_2$ : 32 kg/kmol

100% excess air = 2x stoichiometric air (means exact amount of air to burn)



$\Rightarrow$  Therefore, 1 kmol  $\text{CH}_4$  need 2 kmol  $\text{O}_2$  to burn

$\Downarrow$

$$\frac{3600 \text{ kg/hr } \text{CH}_4}{16 \text{ kg/kmol}} = \frac{1}{2} \times \frac{\text{flow rate of } \text{O}_2}{32 \text{ kg/kmol}}$$

$$\Rightarrow \text{flow rate of } \text{O}_2 = 14400 \text{ kg/hour}$$

$$\Rightarrow \text{Stoichiometric air} = \frac{\text{O}_2}{23.3\%} = 61802.575 \text{ kg/hr}$$

$\Rightarrow$  100% excess air

$$\Rightarrow \text{Flow rate of air} = 61802.575 \times 2 = 123605.15 \text{ kg/hr}$$

Q2 (a) Five Critical Temperature are:

- Cloud point: This is only apply to DMX distillate fuel (solidified). It means the lowest temperature at which wax precipitates as fuel is cooled and this might result to filter blockage. At this point, wax start to crystallise out and clear fuel become opaque.
- Pour point: This is the temperature at which fuel just remain fluid so that fuel can still be pump around. Lower than this point fuel will gel.
- Solidifying point: It's the highest temperature at which fuel remains solid and required warm up.
- Flash point: lowest temperature that air/fuel mixture can be ignite by flame or spark, it's a safety measure to avoid risk. Fuel must be store at least  $10^{\circ}\text{C}$  below. For engine room, flash point must higher than  $60^{\circ}\text{C}$  and for lifeboat must be higher than  $43^{\circ}\text{C}$ .
- Ignition point: Lowest temperature which air fuel mix will spontaneously ignite and maintain a flame for more than 5 seconds.

(b) From the graph, we are able to see that the fuel has density of  $920\text{ kg/m}^3$  at  $15^{\circ}\text{C}$ . Therefore, we are able to find out that at  $80^{\circ}\text{C}$ , its density is  $875\text{ kg/m}^3$   
 40 MW containership with fuel consumption of  $18\text{g/kwh}$  and require 3 week 110% of  $875\text{ kg/m}^3$  fuel oil

$$\Rightarrow \text{consumption} = 40000\text{ kW} \cdot 24\text{h} \cdot 21\text{ days} \cdot 0.18\text{ kg/kwh} \cdot 110\% \\ = 3991680\text{ kg}$$

Because keep at  $875\text{ kg/m}^3$

$$\Rightarrow \text{Volume} = 3991680\text{ kg} / 875\text{ kg/m}^3 = 4561.92\text{ m}^3$$

Q<sub>3</sub> (a) A central cooling system use a close fresh water circuit as coolant to reduce risk of corrosion compare to sea water. Sea water system is limited to a set of pumps, valves and filters. It consist of 3 main parts namely seawater circuit, high temperature circuit and low temperature circuit. Sea water pass valve, cooler and pump overboard. How many pump to open depends on central water temperature.

Advantages of central cooling systems are:

- Corrosion in the fresh water system is eliminated compared to sea water (provided chemical treatment is maintained).
- Component of the system (valves, pipes and coolers) in contact with only fresh water, can be cheaper material.
- Constant temperature of cooling water means easier cooler's control, which means compare to separate system control valve can control mixing.
- Filters and coolers cleaning and maintance are reduced, lesser manpowered for maintance is needed so that cost of manpower can be saved.

Disadvantages of central cooling system:

- Over-heating of one machinery will affect cooling capacity of other machinery. Due to flow is constant so that you are not able to control single component in the whole system.
- Contamination of cooling water caused by one system will affect entire fresh water cooling circuit.
- Initial system design layout is expensive since o/L (outlet) of one system will be i/L (inlet) of another.

$$(b) (i) Q_{out} = m \cdot c \cdot (T_1 - T_2) = 1 \text{ kg/s} \cdot 1400 \text{ J/kg} \cdot \text{K} \cdot (50 - 30) = 28 \text{ kJ/s} \quad \text{--- } 20^\circ\text{C}$$

$$(ii) Q_{oil} = m_{water} \cdot c_{water} \cdot (T_{out} - T_{in}) \Rightarrow 28 \text{ kJ/s} = 0.5 \text{ kg/s} \cdot 4200 \text{ J/kg} \cdot \text{s} \cdot (T_{out} - 20^\circ\text{C})$$

$$\Rightarrow T_{out} = 33.33^\circ\text{C}$$

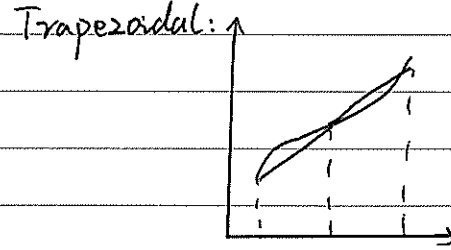
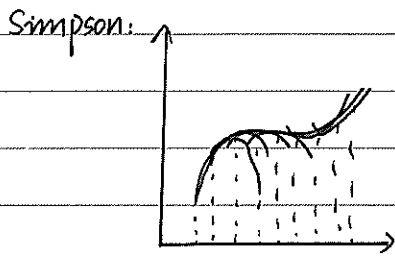
$$(iii) Q = UA\theta_m = 70 \text{ W/m}^2\text{K} \cdot A \cdot 17^\circ\text{C} = 28 \text{ kJ/s} \Rightarrow A = 23.53 \text{ m}^2$$

$$\text{Area} = \text{length} \cdot 10 \text{ mm} \cdot \pi \cdot 200 = 2 \text{ m} \cdot \pi \cdot \text{length} = 23.53 \text{ m}^2 \Rightarrow \text{length} = 3.74$$

$$\therefore \text{length of tube is } 3.74 \text{ m.}$$

Q4 (a)  $A_{wp} = 2 \times \frac{30}{3} \cdot (0.2 + 4 \cdot 2.5 + 12 \cdot 10 + 4 \cdot 15 + 2 \cdot 11 + 4 \cdot 4 + 0.3) = 2570 \text{ m}^2$   
 $I_T = \frac{2}{3} \times \frac{30}{3} \times (0.2^3 + 4 \cdot 2.5^3 + 12 \cdot 10^3 + 4 \cdot 15^3 + 2 \cdot 11^3 + 4 \cdot 4^3 + 0.3^3) = 123203.5667 \text{ m}^4$   
 $TPC = \rho_{\text{seawater}} \cdot A_{wp} \cdot 0.01 \text{ m} = 1025 \text{ kg/m}^3 \cdot 2570 \text{ m}^2 \cdot 0.01 \text{ m} = 26342.5 \text{ t}$

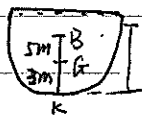
(b) Simpson's rule is more accurate than Trapezoidal rule, <sup>because</sup> Simpson rule use parabola and lesser lines which nearer to actual curve



Usually for a shape of ship, there is curve up section and curve down section. Depending on ship's shape, there is no correct answer for these two which one have higher value result but only can say Simpson's rule is closer to real result and only can be used if we have even sample points. (This question is tricky and I'm not sure whether my answer is correct)

This question need to assume  $B = 15$  !!!

(c)



$d = 7 \text{ m}$

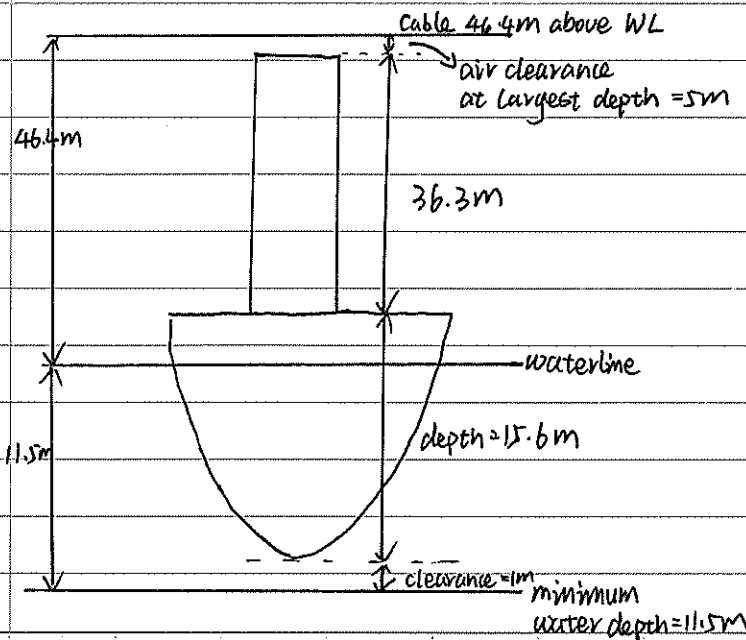
$C_b = \frac{\nabla}{BTL}$  ,  $BM_T = \frac{I_t}{\nabla} = \frac{I_t}{BTL \cdot C_b}$

$\Rightarrow \therefore I_t = 123203.5667 \text{ m}^4$  ,  $B = 15 \cdot 2 = 30 \text{ m}$  ,  $L = 30 \cdot 6 = 180 \text{ m}$

$\therefore BM_T = \frac{123203.5667}{15 \cdot 2 \cdot 7 \cdot 180 \cdot 0.6} = 5.43 \text{ m}$

$\therefore GM_T = (KB - KG) + BM_T = 5.43 + (5 - 3) = 7.43 \text{ m}$ .

Q5.



ship total =  $36.3 \text{ m} + 15.6 \text{ m} = 51.9 \text{ m}$

largest draft =  $11.5 \text{ m} - 1 \text{ m} = 10.5 \text{ m}$

Air draft =  $51.9 \text{ m} - 10.5 \text{ m} = 41.4 \text{ m}$

$\therefore$  Clearance =  $46.4 - 41.4 = 5 \text{ m}$

Qb. (a) Ship resistance are consist of:

- Water resistance which consist of frictional resistance (no static form, have dynamic friction), wave breaking resistance (sea is not clam) and wave making resistance (move in water create wave means loss of energy).
- Air resistance: much lesser than water resistance, it's negligible.

(b) The reasons are:

- Ships will slowly have wear and tear
- Fuel consumption will increase as engine efficiency reduced and fouling
- Over heating problem occur as system wear and tear.
- Anti fouling paint failure which increase resistance.
- Heating and cooling system break down
- Self-polishing paint wear off.
- Wear and tear of lub oil
- Wear and tear of cylinder liner, engine crank case and piston etc which cause inefficient combustion or crank case explosion.

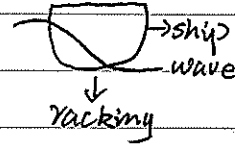
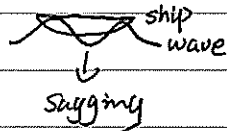
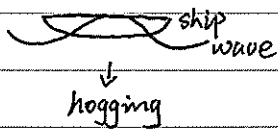
(c) The ship build in Japan, <sup>usually</sup> will be most expensive follow by Korea and China is least expensive.

The reason for the price different are:

- The types of ship they build. For example, dry bulk is popular in Japan
- Concept in people's mind that Japan has best quality and China has worse.
- Reputation of ship yard.
- Your bargaining power and specific design requirement.
- How close you are with the shipyard.
- Shipping market and how urgent you are.
- Are you booking a series of ships.
- How your ordering can fit into shipyard's building schedule
- Shipyard capacity

Q7 (a) If it's head sea which means ship will encounter sagging and hogging deformation.

If it's beam sea, deformation called racking will occur



(b) Ship structure overcome these deformation using high tensile steel or casting iron and also, use plating and stiffening longitudinal and transversely to enhance the strength of the ship. Net-work are welded together.

(c) (i) The factors are:

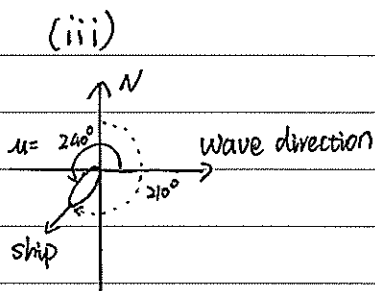
- After keel laying, change of width which affect original plan for vessels.
- Put <sup>more</sup> heavy fire arms on higher deck which result in reduce of stability as  $G$  goes up and  $GM$  reduce
- Heavy oak cavings outfit in upper deck further move  $G$  center up and reduce  $GM$ .
- No room for ballast water to help stabilize the ship.

This Q is lack of one data that "C=0.38"

(ii) Assumption: the ship motion is assumed to be simple harmonic motion and experience liner restoring force.

$$T_{roll} = \frac{2C \times B}{\sqrt{GM_T}} \Rightarrow GM_T = \left( \frac{2C \times B}{T_{roll}} \right)^2, \because C=0.38, B=5m, T=10.55$$

$$\therefore GM_T = \left( \frac{2 \times 0.38 \times 5}{10.55} \right)^2 = 0.131 \text{ m.}$$



$$\Rightarrow W_e = W - \frac{W^2}{g} \cdot V \cdot \cos \mu, T=12 \text{ second}, W = \frac{2\pi}{T} = \frac{\pi}{6} \text{ rad/s}$$

$$W_e = \frac{\pi}{6} - \frac{(\frac{\pi}{6})^2}{9.8} \cdot 10 \text{ knots} \cdot \cos 240^\circ = 0.66 \text{ rad/s}$$

$$\therefore T_e = 9.525 \quad T_{roll} = 10.55$$

Therefore, Wave period in counter is close to period of roll motion. Resonance will happen and its amplitude is huge compare to pitch and heave which might lead to