

# GEOTECHNICAL ENGINEERING ( May / June 2017)

No. :

Date :

i) a) same normal stress = 200 kPa  
 peak shear stress → 150 kPa  
 → 180 kPa

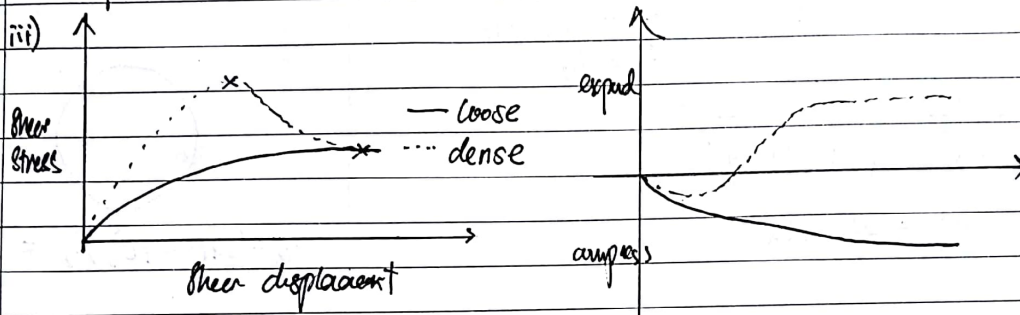
i) sand ⇒ c' = 0

$$\tau = \sigma_n \tan \phi'$$

$$\phi' = 36.87^\circ$$

$$\phi'' = 41.99^\circ$$

ii) friction angle of ultimate state of dense sand is loose sand's friction angle.  
 $\phi_{\text{ultimate, dense}} = 36.87^\circ$



### Advantages:

- simple and relatively simple to construct
- normal and shear stresses were measured directly.
- imposed a plane strain condn

### Disadvantages:

- failure plane is forced.
- drainage isn't controlled
- lateral stress not known.

b)  $\sigma_3 = 200 \text{ kPa}$

i)  $w_i = 55\%$

max axial load = 800 N

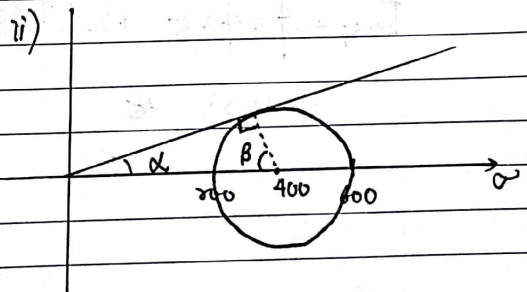
cross. s. Area = 2000 mm<sup>2</sup>

normal axial stress at failure = 400 kPa

$$\sigma_1 = 400 \text{ kPa} + 200$$

$$= 600 \text{ kPa}$$

$$q = 600 - 200 = 400 \text{ kPa}$$



ii)  $R = 200$       $\tau_f = \sin \beta$   
 $\alpha = 30^\circ$       $R$   
 $\beta = 60^\circ$       $\tau_f = 100 \text{ kPa}$   
 $\tau_f = \frac{100}{R} = \sin \beta$   
 $\sigma_f = 400 - 173.2 = 226.8 \text{ kPa}$       $\sigma = \cos \beta$   
 $\sigma = 173.205$

iv) effective ~~friction~~ friction angle  $\Rightarrow \phi' = 30^\circ$

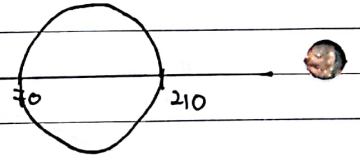
v) water content at the end of the test decreases.  
as  $w = \frac{M_w}{M_s}$ , NC soil will be compacted at end of the test,  
which decreases the void ratio and thus decreasing  
water content.

c.)  $\phi' = 30^\circ$   $p_{opp} = 130 \text{ kPa}$

$$\sigma_3^f = 200 \quad \sigma_3^i = 200 - 130 = 70$$

$$\frac{\sigma_1^i}{\sigma_3^i} = \left( \frac{1 + \sin \phi'}{1 - \sin \phi'} \right)$$

$$\sigma_1^i = 210 \text{ kPa}$$

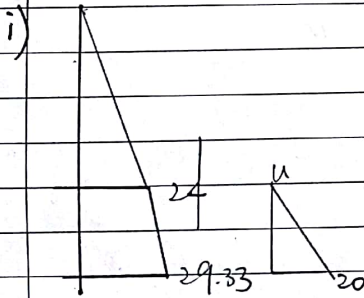


$$c_u = (210 - 70) / 2 = 70 \text{ kPa}$$

2.) a.) Use Rankine's

$$\gamma_w = 10 \text{ kN/m}^3$$

$$K_A = \left( \frac{1 - \sin \phi'}{1 + \sin \phi'} \right) = \frac{1}{3}$$



$$\sigma_{h'} = \frac{1}{3} \sigma_2'$$

$$\sigma_{2,4m}' = 4 \times 18 = 72$$

$$\sigma_{h,4m}' = 24$$

$$\sigma_{216}' = 6 \times 18 - 2(10) = 88$$

$$\sigma_{h16}' = 29.33$$

$$T_{\text{total}} = 24 \times 4 \times \frac{1}{2} + \frac{(29.33 + 24) \times 2}{2} + \frac{20 \times 2}{2}$$

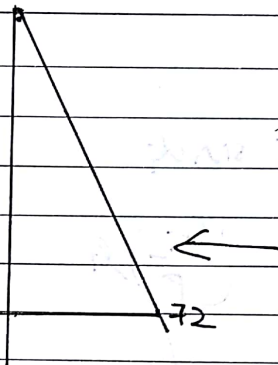
$$= 121.33 \text{ kN}$$

ii)

$$\sigma_H = \sigma_z = -2cu$$

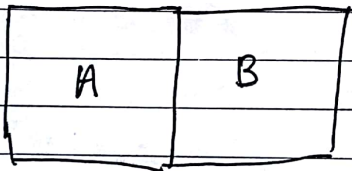
$$\begin{aligned} \sigma_{\text{Ar6m}} &= \sigma_{z,6m} - 2cu \\ &= 6(18) - 2(18) \\ &= 72 \end{aligned}$$

$$\begin{aligned} \tau_{\text{max}} &= 72 \times 6/2 \\ &= 216 \end{aligned}$$



iii)  $\Rightarrow$  It will be the same as total strength <sup>analysis is not influenced</sup> ~~do not~~ by water pressure.

b.)



$$B = L = 10 \quad z = 5$$

$$m = n = 2$$

$$I_r = 0.232$$

$$\Delta \sigma_{z,A} = 40 \times 0.232 = 9.28$$

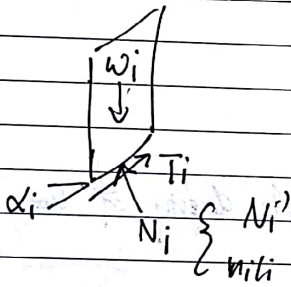
$$\Delta \sigma_{z,B} = 13.92$$

$$\Delta \sigma_z = 23.2 \text{ kPa.}$$

$$(ii) \quad F = \frac{10(33) + \tan(33)(1060)}{1030}$$

$$= 0.9887 \rightarrow \text{failure.}$$

- iv) Fellemus : resultant interlice force = 0  
 Brelap : assume  $X_1 - X_2 = 0$   
 Sprener : assume forces acted in parallel direction.
- } different assumptions caused the difference



$$N_i - W_i \cos \alpha_i = 0$$

$$N_i' + T_i' - W_i \cos \alpha_i = 0$$

$$N_i' = W_i \cos \alpha_i - T_i'$$

$$F = \frac{a^2 L a + \tan \phi' \sum_i (W_i \cos \alpha_i - T_i')}{\sum_i W_i \sin \alpha_i}$$

4)

a.i.

- Cover soil with temporary surcharge
- Cause soil to consolidate, thus improving settlement and strength properties
- Once desired properties have been obtained, surcharge is removed
- Typically 3 to 8 m thick

ii. consolidation, process reduces porewater pressure

- As  $\sigma' = \sigma - u$
- If  $u$  decreases,  $\sigma'$  increases
- And if  $\sigma'$  increases, shear strength increases

b.i. silt content < 12-15%  
clay content < 3 %

ii. loose sand can be densified using vibro compaction.  
Density is a factor of sand strength property  
As density of loose sand increases, the shear strength will be increased

c.i. At low water content, water acts as lubricant, allowing particles to be packed closer, resulting a higher dry density

At high water content, water starts to replace particles as particles cant be packed anymore closer by means of water.

As unit weight of water is lower than soil particles, the dry unit weight decreases as water content increases above the optimum

ii. Dry of optimum – particles are arranged in flocculated manner.  
Wet of optimum – particles are arranged in oriented fabric manner

Dry :

- higher shear strength even with the same dry unit weight
- higher hydraulic conductivity

Wet :

- lower hydraulic conductivity

d.

i. Horizontal drains helps to dissipate porewater pressure and lower ground water table

- As  $\sigma' = \sigma - u$
- If  $u$  decreases,  $\sigma'$  increases
- And if  $\sigma'$  increases, shear strength increases

ii. piezometer can be installed before the installation of horizontal drains

initial ground water level can be determined

after the installation of the horizontal drains, piezometers can be used to record the changes in ground water table. Thus, observing the performance of the horizontal drains.

$$\begin{aligned}
 e_i) \quad D_r &= 0.3 & 0.3 &= \frac{l_{max} - e_i}{l_{max} - l_{min}} & 0.9 &= \frac{l_{max} - e_f}{l_{max} - l_{min}} \\
 l_{max} &= 0.9 & & & & \\
 l_{min} &= 0.3 & & & & \\
 & & e_i &= 0.72 & e_f &= 0.36
 \end{aligned}$$

- ii) since the fill is a 10m thick loose sand fill  
 vibrocompaction method can be used for the densification process.
- can be done by inserting vibratory probe into ground.
  - ~~either~~ <sup>2</sup> most commonly used  $\rightarrow$  terra probe and vibroflot.
  - both method densify the sand fill using vibration ~~method~~.