

1 a) T_1 can be decomposed into three parts

$$L_{BC} = \sqrt{3^2 + 4^2 + (4+2+3)^2} = \sqrt{106}$$

$$\vec{T}_1 = \frac{4}{\sqrt{106}} T_1 \hat{i} + \frac{3}{\sqrt{106}} T_1 \hat{j} - \frac{9}{\sqrt{106}} T_1 \hat{k}$$

$$\vec{r}_{AB} = 0\hat{i} + 0\hat{j} + 9\hat{k}$$

$$\vec{M}_{T_1} = \vec{r}_{AB} \times \vec{T}_1$$

$$\vec{M}_{T_1} = 9\hat{k} \left(\frac{4}{\sqrt{106}} T_1 \hat{i} + \frac{3}{\sqrt{106}} T_1 \hat{j} - \frac{9}{\sqrt{106}} T_1 \hat{k} \right)$$

$$\vec{M}_{T_1} = \frac{36}{\sqrt{106}} T_1 \hat{j} - \frac{27}{\sqrt{106}} T_1 \hat{i} + 0\hat{k}$$

$$\vec{M}_{T_1} = -\frac{27}{\sqrt{106}} T_1 \hat{i} + \frac{36}{\sqrt{106}} T_1 \hat{j} + 0\hat{k} = -2.622 T_1 \hat{i} + 3.495 T_1 \hat{j}$$

b) $\vec{M}_{T_2} = 0\hat{i} - 6T_2 \hat{j} + 0\hat{k}$

$$\vec{M}_{30kN} = 120\hat{i} + 0\hat{j} + 0\hat{k}$$

$$\sum \vec{M}_A = 0$$

$$\vec{M}_{T_1} + \vec{M}_{T_2} + \vec{M}_{30kN} = 0$$

$$\left(-\frac{27}{\sqrt{106}} T_1 + 120 \right) \hat{i} + \left(\frac{36}{\sqrt{106}} T_1 - 6T_2 \right) \hat{j} + 0\hat{k} = 0$$

$$\Downarrow$$

$$T_1 = 120 \times \frac{\sqrt{106}}{27}$$

$$T_1 = 45.758 \text{ kN}$$

$$\Downarrow$$

$$T_2 = \frac{6}{\sqrt{106}} \times 120 \frac{\sqrt{106}}{27}$$

$$T_2 = 26.667 \text{ kN}$$

c) $\Sigma F = 0$

$$\vec{A} + \vec{T}_1 + \vec{T}_2 + (-50\hat{j}) = 0$$

$$\vec{A} = -\left(\frac{4 \times 120}{27} \hat{i} + \frac{3 \times 120}{27} \hat{j} - \frac{9 \times 120}{27} \hat{k}\right) - \left(-\frac{6 \times 120}{27} \hat{i}\right) - (-30\hat{j})$$

$$\vec{A} = \underbrace{8.889}_{A_x} \hat{i} + \underbrace{16.667}_{A_y} \hat{j} + \underbrace{40}_{A_z} \hat{k}$$

2a) $M_A = 0$

$$4 \times 3 \times \frac{3}{2} + 24 - 12 \times 8.5 + V_E \times 10 = 0$$

$$V_E = 6 \text{ kN} \downarrow$$

$$\Sigma F_y = 0$$

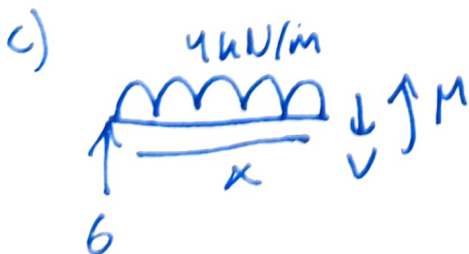
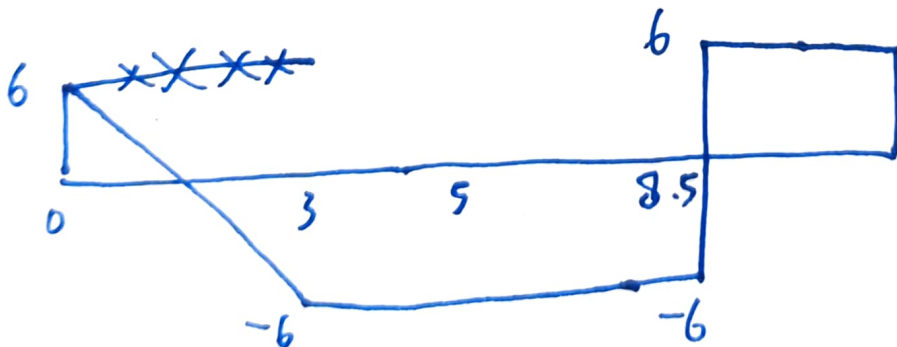
$$V_A - 4 \times 3 + 12 - 6 = 0$$

$$V_A = 6 \text{ kN} \uparrow$$

$$\Sigma F_x = 0$$

$$H_A = 0 \text{ kN}$$

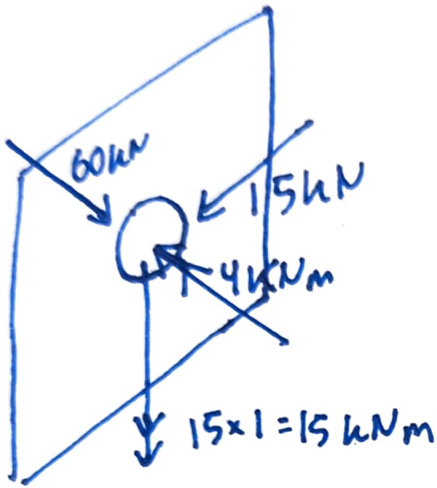
b) SFD



$$M = 6x - 4x \cdot \frac{x}{2}$$

$$M = 6x - 2x^2 \quad (0 \leq x \leq 3)$$

3a)



b) $\theta = \frac{TL}{GJ}$

$\theta = \frac{(4 \times 10^6) \times (500)}{(90 \times 10^3) \times (\frac{1}{2} \pi \times 150^4)} \times \frac{180}{\pi}$ ↗ convert to degree

$\theta = 0.0016$ degree counter clockwise

c) Normal due to 60kN axial

$\sigma = \frac{60000}{\pi \times 150^2} = 0.849 \text{ MPa}$

Normal due to 15kNm moment

$\sigma = \frac{My}{I} = 0 \quad (y=0)$

Shear due to 4kNm torsion

$\tau = \frac{(4 \times 10^6) \times (150)}{\frac{1}{2} \pi \times 150^4} = 0.755 \text{ MPa} (\leftarrow)$

Shear due to 15kN

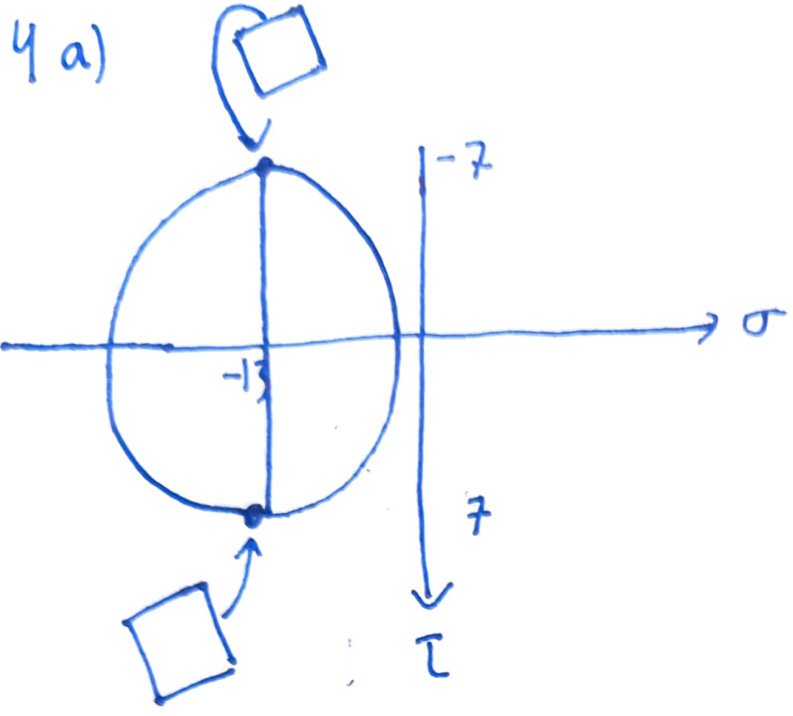
$\tau = \frac{15000 \times \frac{1}{2} \pi \times 150^2 \times \frac{4 \times 150}{3\pi}}{\frac{1}{4} \pi \times 150^4 \times 300}$

$\tau = 0.283 \text{ MPa} (\rightarrow)$

Resultant

$\sigma = 0.849 \text{ MPa}$

$\tau = 0.472 \text{ MPa} (\leftarrow)$

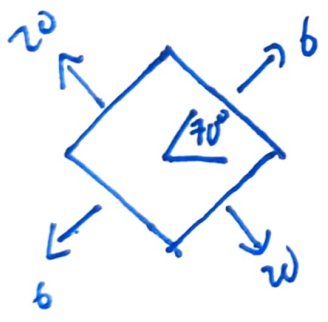


principal stresses

$$\sigma_1 = -13 + 7 = -6 \text{ MPa tensile}$$

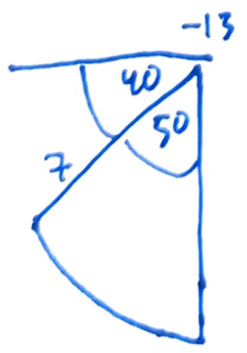
$$\sigma_2 = -13 - 7 = -20 \text{ MPa tensile}$$

turn $\frac{90}{2} = 45$ degree from 25° (either way)



turn 25 degree clockwise from 25° to get 0°

$25 \times 2 = 50$ degree CW turn in Mohr circle

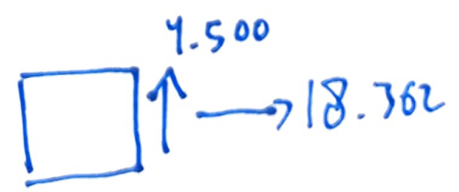


$$\sigma = -13 - 7 \cos 40$$

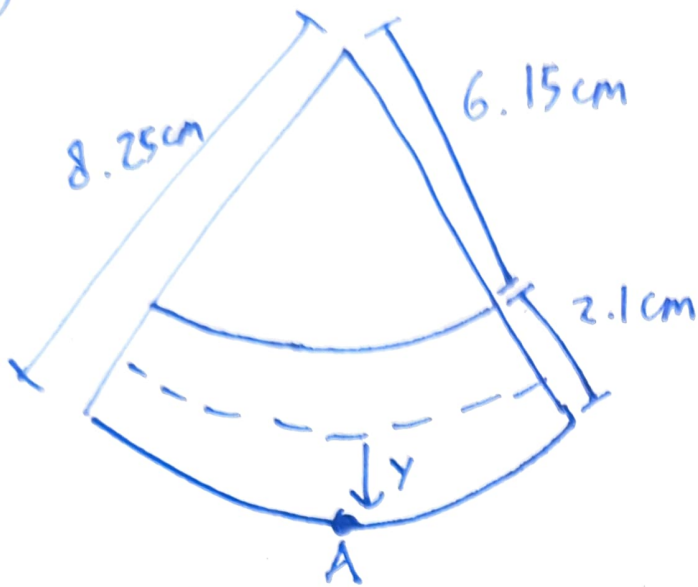
$$\sigma = -18.362 \text{ MPa}$$

$$\tau = 7 \sin 40$$

$$\tau = 4.500 \text{ MPa}$$



4b)



$$R = \frac{8.25 + 6.15}{2} = 7.2 \text{ cm} = 72 \text{ mm}$$

at point A

$$\epsilon = \frac{y}{R}$$

$$\sigma = E \epsilon$$

$$\frac{M y}{I} = E \frac{y}{R}$$

$$M = \frac{E I}{R}$$

$$M = \frac{25 \times \frac{1}{12} \times 21^4}{72} \times 10^{-3}$$

square $b = h$

$$M = 5.627 \text{ Nm}$$